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Mixed Matrix Membranes Based on Metal–Organic Frameworks with Tunable Pore Size for CO₂ Separation

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Supporting Information

ABSTRACT: Two isomorphous MOFs (Ni₂(L-asp)₂bipy and Ni₂(L-asp)₂pz) with different pore sizes were incorporated into poly(ether-block-amide) (Pebax-1657) to prepare the mixed matrix membranes (MMMs) with gas permeation properties for CO_2 , H_2 , N_2 , and CH_4 . Different loading ratios of MOFs with mass percentage from 10% to 30% were studied. Compared with the pure polymer membrane, the assynthesized two series of MMMs showed improved CO₂ permeability and CO_2/H_2 selectivity. The highest CO_2 permeation property was achieved by Ni₂(L-asp)₂bipy@ Pebax-20 of 120.2 barrers with an enhanced CO_2/H_2



selectivity of 32.88 compared with 55.85 barrers and 1.729 of the pure polymer membrane, respectively, which makes it a potential candidate for future applications in CO₂ capturing.

1. INTRODUCTION

The rising of population and explosive growth in energy consumption results in the enhancement of CO₂ content in the atmosphere, which probably causes a series of changes in human life.¹ CO₂ gas accounts for about 60% of the effect of greenhouse gases on global climate change.² To reduce CO₂ content, there are three main strategies, such as improving the efficiency of energy utilization, searching for new clean and renewable energy sources, and, more importantly, developing CO₂ capture technologies. Nowadays, both precombustion and postcombustion CO₂ captures need separation of CO₂ from other gas molecules.^{2,3} Some technologies have been developed to capture and separate CO2, including amine absorption process,^{4,5} dual-alkali absorption approach,⁶ molecular sieve adsorbent,^{7,8} and cryogenic separation. However, most of these processes require high energy consumption to be carried out. Therefore, it is urgent to develop an alternative, cost-effective, and low energy consumption technology for CO₂ removal, such as membrane based separation.⁹⁻

Membranes have been widely used in various industrial separations for the past decades.^{9,13-16} Industrial applications are currently dominated by polymeric membranes.¹⁷⁻²⁰ Generally, advantages of using polymeric materials as membranes include: light weight, processability into different morphologies (such as thin films, porous beads, hollow fibers, and composites), and variations in structure and properties.²¹ For polymer membrane based gas separation, a trade-off between selectivity and permeability usually appears, which is due to the nature of polymer materials.^{22,23} To solve this issue, microporous fillers have been involved into the polymer matrix to form mixed matrix membranes (MMMs).24-26 In the

pioneering work, zeolites were used as fillers to combine with polymers to give improved gas separation performances compared with pure polymer membranes.²⁴ However, the weak interaction between inorganic filler and polymer phase usually leads to a rigidified interface or sieve-in-cage structure that holds back the performance enhancement of zeolite based MMMs. To this end, application of new microporous fillers that can improve the interaction with polymer phase is vital to the performance enhancement of the MMMs.

Metal-organic frameworks (MOFs) are a merging group of nanoporous materials constructed from inorganic metal centers and organic linkers, which have attracted great research interests in the fields of separation and adsorption due to their well-defined pores, large surface areas, and tunable pore sizes and chemical environment.^{27–33} Recent experimental efforts have led to the conclusion that MOFs used as fillers are more compatible with polymers since MOFs possess organic linkers in the structure that can enhance the adhesion to polymer phase.^{34–38} Furthermore, in the study reported by Long et al., MOF fillers can help polymers to overcome the issue of plasticization conversely.

Due to the advantage of tunable pore sizes, in this work, we report on the design and fabrication of MMMs based on MOFs with different pore sizes for CO₂ capture application. A kind of commercial polyether block amide Pebax MH 1657 (Pebax) was used as the polymer matrix (Figure S1).⁴⁰⁻⁴² Two isomorphous MOF frameworks, Ni₂(L-asp)₂bipy and Ni₂(L-

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asp)₂pz (L-asp = L-aspartic acid, bipy = 4,4'-bipyridine, and pz = pyrazine), were chosen as fillers with a window size of 3.8 × 4.7 Å and 2.5 × 4.5 Å, respectively. The difference in pore size is brought by the different lengths of organic linker. These two MOFs were combined with Pebax polymer and made into MMMs with different loading amount.^{12,43} The obtained MMMs were characterized by powder X-ray diffraction (PXRD), scanning electron microscope (SEM), thermogravimetric analysis (TGA), and Fourier transform infrared spectroscopy (FTIR). The gas permeability of MMMs was also tested, and the results showed that the introduction of Ni₂(L-asp)₂bipy and Ni₂(L-asp)₂pz improved the CO₂ permeability and CO₂/H₂ selectivity of the polymer membrane.

2. MATERIAL AND METHODS

2.1. Synthesis of MOF Crystals. Both $Ni_2(L-asp)_2$ bipy and $Ni_2(L-asp)_2pz$ crystals were synthesized by the conventional solvothermal method. First, $NiCO_3 \cdot 2Ni(OH)_2 \cdot xH_2O$ (2.450 g) and L-aspartic acid (2.630 g) were dissolved in water (200 mL) under stirring and heating for 3 h. After filtering out all the remaining solid particles, the clear turquoise solution was then evaporated at 80 °C in an oven overnight to obtain the Ni(L-asp) powder. For the synthesis of $Ni_2(L-asp)_2$ bipy MOF, a mixture of Ni(L-asp) (0.22 mmol), bipy (0.49 mmol), H_2O (6 mL), and methanol (6 mL) was sealed in the autoclave and heated in a 150 °C oven for 24 h. For the synthesis of $Ni_2(L-asp)_2pz$ MOF, the same conditions were applied, while 4,4′-bipyridine was replaced by the same moles of pyrazine. The green MOFs powders were filtered and washed several times with a solution of water/methanol (1:1, v/v) to remove the unreacted reagents and then dried in a 60 °C oven.

2.2. Preparation of MMMs with Different Loading of MOFs Fillers. A certain amount of $Ni_2(L-asp)_2$ bipy or $Ni_2(L-asp)_2pz$ crystals were ground and dispersed in ethanol and water mixed solution with a mass ratio of 7:3, followed by sonication and stirring for 10 min, respectively. The obtained suspension was mixed with Pebax polymer and refluxed under 80 °C for 12 h. The loading amount of MOFs was varied from 10% to 30%, while the mass ratio of Pebax and solvent was 5:95. The final mixed solution was casted on a flat glass substrate. After the evaporation of ethanol and water in the air for 12 h and then in vacuum for 24 h at 40 °C, the prepared $Ni_2(L-asp)_2$ bip@Pebax-x and $Ni_2(L-asp)_2pz@Pebax-x$ (where x represents the mass percentage of MOF fillers) were ripped off carefully from the glass substrate for characterization and gas permeability tests.

2.3. Characterizations. Information about the crystalline structure of the MOFs and MMMs was collected on a Bruker AXS D8 Advance instrument. The microscopic features of these membranes were characterized by a scanning electron microscope (JEOS JSM-6510A). The optical photos of the membranes were taken by a mobile phone at normal camera mode. The Fourier transform infrared spectroscopy (FTIR) spectra of membrane materials were collected by Spectrum One, and thermal gravimetric analysis on materials was carried out by a TGA/DSC1Mettler Toledo.

2.4. Gas Permeability Test. The MMMs were tested for their H_2 , CO_2 , N_2 , and CH_4 pure gas permeation properties. Pure gas measurements were carried out using a variable pressure constant-volume gas permeation cell technique. The permeation cell setup and testing procedures had been described elsewhere.¹ The operating temperature was 35 °C, and the upstream gauge pressure was 1 atm. The gas permeability was calculated from the rate of pressure increasing (dp/dt) at a steady state according to the following eq 1

$$P = \frac{273 \times 10^{10}}{760} \frac{VL}{AT(p_2 \times 76/14.7)} \left(\frac{dp}{dt}\right)$$
(1)

where *P* is the membrane gas permeability in barrers (1 barrer = 1×10^{-10} cm³(STP)·cm·cm⁻²·s⁻¹·cmHg⁻¹), *V* represents the volume of the downstream reservoir (cm³), A is the effective membrane area

(cm²), *L* refers to the membrane thickness (cm), *T* is the operating temperature (K), and p_2 indicates the upstream pressure (psia). The ideal permselectivity was calculated based on the following eq

2:

$$\alpha(i/j) = \frac{P_i}{P_j} \tag{2}$$

3. RESULTS AND DISCUSSION

3.1. Membrane Characterizations. As shown in Figure 1, two isomorphous MOF frameworks Ni₂(L-asp)₂bipy and



Figure 1. Schematic illustration of the MMMs structure and the possible gas transport mechanism.

Ni₂(L-asp)₂pz with different pore sizes were used as fillers in this work. The structures of the MOF fillers and the corresponding MMMs with different MOF loading amounts were characterized by powder X-ray diffraction in the range from 4° to 40° (Figure 2). As can be seen, the diffraction peaks of the as-synthesized MOF fillers are in accordance with the simulated patterns, indicating their good crystallinity and phase purity. Though the pure polymer shows an amorphous structure with no obvious peaks, the typical features of the MOF fillers appear in the patterns of MOFs@Pebax MMMs as expected. The strong peak at a 2θ angle of 16.7° in Figure 2a is associated with the (1 1 0) crystal plane of Ni₂(L-asp)₂bipy, which indicates that the Ni₂(L-asp)₂bipy particles were incorporated in the membrane with a preferential crystal orientation. It may be an important factor determining the separation performance of the Ni₂(L-asp)₂bipy@Pebax MMMs. The intensity of the diffraction peaks in both series of MMMs becomes stronger when the loading amount of MOF fillers increases, which also indicates that the structure of MOF fillers is maintained well in the MMMs.

The pure polymer Pebax membrane is colorless (Figure S2) and shows a smooth surface (Figure 3b). After incorporation of MOF fillers, as shown in the optical picture of membrane Ni₂(L-asp)₂bipy@Pebax-20 (Figure 3a), the membrane turns to light green and the surface becomes rough (Figure 3c). The membrane layer is composed of MOF particles and polymer, and the thickness of the membrane is determined to be 90-110 μ m. Closer inspection of the respective MMM cross section reveals that there is macroscopic plastic deformation seen as polymer veins. It therefore suggests an even distribution of MOFs fillers in the polymer matrix. The formation of these veins is due to plastic deformation, which has also been seen in other MOF based MMMs and attributed to a strong interaction between the polymer and the fillers.² Other membranes with different MOF loading amounts were also characterized in the same manner, and the SEM images are shown in the Supporting Information (Figures S3 and S4).



Figure 2. PXRD patterns of the simulated and as-synthesized MOF fillers, pure polymer Pebax, and the corresponding MMMs with different loading amounts of MOF fillers.



Figure 3. (a) Optical image of membrane $Ni_2(L-asp)_2bipy@Pebax-20$. SEM images of (b) the pure polymer Pebax membrane, (c) the top view and (d) cross section of membrane $Ni_2(L-asp)_2bipy@Pebax-20$.

The structural stability and integrity of MOF fillers and the MMMs were studied by TGA (Figure 4a,b). The slight weight loss of the Ni₂(L-asp)₂bipy and Ni₂(L-asp)₂pz powders from 100 to 200 °C can be attributed to the removal of absorbed water. Both of the MOF fillers exhibit a decomposition temperature above 350 °C, which has even been increased to around 400 °C after incorporated in the Pebax polymer due to the strong interaction between the MOF fillers and the polymer matrix. These results prove that the as-synthesized MMMs are quite stable for industrial application such as gas separation. FTIR tests were also carried out on the pure polymer membrane and the MMMs (Figure 4c,d). For the pure polymer membrane, the peaks of 1100 and 1640 cm⁻¹ are referred to the ester groups, while the peaks of 1545 and 3300 cm⁻¹ can be assigned to the methylene and amine of the Pebax, respectively. Compared with the pure polymer membrane, new peaks of 865, 1422, and 1576 cm⁻¹ are detected according to the organic ligands of MOF fillers, which further proves the successful incorporation of MOF fillers in the Pebax polymer.

3.2. Gas Permeability. Single gas permeation experiments of H_2 , N_2 , CO_2 , and CH_4 for the pure polymer membrane and the two series of MOFs@Pebax MMMs were carried out, and the results are summarized in Figure 5 and Tables S1 and S2. It can be seen that the presence of MOFs strongly affects the gas

transport properties of the membranes. For the membranes using $Ni_2(L-asp)_2$ bipy as the filler (Figure 5a), the CO₂ permeability increases significantly compared with the pure polymer, and the highest permeability is obtained when the loading amount reaches 20%. The membrane of Ni₂(Lasp)₂bipy@Pebax-20 possesses permeability around 120 barrers, which is twice as much as that of the pure polymer. The enhancement of permeability can be attributed to strong affinity for CO₂ molecules of the $Ni_2(L-asp)_2$ bipy structure, which facilitates their diffusion and thus enhances the permeability. The reduced crystallization and free volume introduced by incorporation of Ni₂(L-asp)₂bipy also make the transport of CO₂ easier through the membrane.⁴⁴ When the loading amount of Ni₂(L-asp)₂bipy increases to 30%, a decrease of CO₂ permeability appears for some degree of membrane inhomogeneity brought by preparation difficulty, which limits the effect of the MOF fillers.

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As shown in Figure 5a, the permeability of H₂ is obviously suppressed by Ni₂(L-asp)₂bipy incorporation and changes slightly with the increase of the filler loading amount. That is because the Ni₂(L-asp)₂bipy particles present a preferential crystal orientation in the membrane certified by XRD results. Along the $\begin{bmatrix} 1 & 1 & 0 \end{bmatrix}$ direction, there are no structural pores (Figure S5b) and the transport of H₂ molecules is blocked, which thus decreases the H₂ permeability. Basing on the sorption-diffusion mechanism, it is different from CO₂ for the reason that CO₂ can be strongly adsorbed by the Ni₂(Lasp)₂bipy framework pores from other directions. The permeability of N₂ and CH₄ changes not much due to the larger kinetic diameter of N_2 (3.6 Å) and CH_4 (3.8 Å) compared to CO_2 (3.3 Å). Corresponding ideal selectivities are calculated based on the permeance results (Figure 5c). Compared with the pure polymer membrane, the CO_2/H_2 selectivity of Ni₂(L-asp)₂bipy@Pebax-20 is greatly enhanced to 32.88 from 1.73, surpassing many of the reported membranes (Table S4), while the CO_2/N_2 selectivity is increased to 52 under 30% loading amount and the CO₂/CH₄ selectivity is well held when the loading amount reached 20% and 30%, respectively. Binary gas mixture $(CO_2/H_2, CO_2/N_2, and CO_2/N_2)$ CH₄) permeation properties were further investigated on Ni₂(L-asp)₂bipy@Pebax-20 membrane, and similar separation performances were obtained (Figure S6 and Table S3). The permeability of CO₂ is a little lower than the single gas tests due to the blocking effect brought by the other kind of gas



Figure 4. TGA curves of the two MOF fillers (a) $Ni_2(L-asp)_2$ bipy and (b) $Ni_2(L-asp)_2pz$ based MMMs. Corresponding FTIR spectra of (c) $Ni_2(L-asp)_2pz$ based MMMs.



Figure 5. Single gas permeability of the two MOF fillers (a) $Ni_2(L-asp)_2bipy$ and (b) $Ni_2(L-asp)_2pz$ based MMMs. Corresponding ideal selectivity of (c) $Ni_2(L-asp)_2bipy$ and (d) $Ni_2(L-asp)_2pz$ based MMMs.

molecules, which contributes to the slight reduction of CO $_2/$ H $_2$, CO $_2/N_2$, and CO $_2/CH_4$ selectivity.

In the case of $Ni_2(L-asp)_2pz$ as the filler, the CO_2 permeability is not increased as high as the $Ni_2(L-asp)_2$ bipy based membranes and even declined when the loading amount was 10%. This is mainly due to the more effective sieving effect played by the small window size of $Ni_2(L-asp)_2pz$. The kinetic

diameter of CO₂ is larger than the window size; however, they still can be adsorbed by the Ni₂(L-asp)₂pz framework owing to its flexibility. The transport of CO₂ is constrained to some extent, resulting in reduced permeability than that of Ni₂(Lasp)₂bipy based membranes. Without the special affinity, even smaller as H₂ cannot enter and move freely in the pores of Ni₂(L-asp)₂pz in the MMM. So it is harder for N₂ and CH₄



Figure 6. Comparison of (a) CO_2/H_2 , (b) CO_2/N_2 , and (c) CO_2/CH_4 separation performance of the as-synthesized and reported MMMs based on MOFs with Robeson's upper bound line (data selected from Tables S1, S2, and S4).^{9,45-52}

with larger kinetic diameters. The permeability fluctuations of H_2 , N_2 , and CH_4 with varied $Ni_2(L-asp)_2pz$ loading amounts are mainly caused by the free volume introduced after MOF incorporation. Accordingly, degraded ideal selectivities of CO_2/H_2 , CO_2/N_2 , and CO_2/CH_4 are detected for nearly all the $Ni_2(L-asp)_2pz$ @Pebax MMMs.

The separation performances of the pure Pebax membrane, the Ni₂(L-asp)₂bipy and Ni₂(L-asp)₂pz based MMMs were also compared with the well-known Robeson upper bound. As shown in Figure 6, the two MOF fillers offer substantial improvement in CO₂ permeability (increased by 115% for Ni₂(L-asp)₂bipy@Pebax-20 and 60.5% for Ni₂(L-asp)₂pz@ Pebax-20) over the pure Pebax membrane. Compared with other reported MOF-based MMMs, the membranes fabricated in this work exhibited well-balanced performance with higher CO₂/H₂ selectivity and intermediate permeability. More importantly, the comparison of the results of these two series of MMMs proves that the tunable pore sizes of the fillers play an important role in regulating the membrane properties, including the permeability and selectivity. The Ni₂(L-asp)₂bipy MOF with larger pore size can provide additional fractional free volume for gas diffusion, resulting in increased diffusion coefficient; thus, the CO₂ permeability of Ni₂(L-asp)₂bipy@ Pebax-20 is greatly improved compared with the pristine Pebax membrane. On the other hand, the window of $Ni_2(L-asp)_2pz$ is too small to let CO₂ molecules pass through, leading to the lower increase of CO₂ permeability for Ni₂(L-asp)₂pz@Pebax MMMs. The different sieving effects brought by fillers with different pore sizes may be an important point to be considered in future MMMs fabrication.

4. CONCLUSIONS

In summary, Pebax was chosen as the matrix to prepare mixed matrix membranes via incorporation of two isomorphous MOFs with different pore sizes. The loading ratio was varied from 10% to 30%. PXRD, SEM, FTIR, and TGA tests were carried out to characterize the structure, morphology, and stability of the obtained membranes. For the gas transport property, MOFs based membranes show improved CO_2 permeability and CO_2/H_2 selectivity compared with the pure polymer membrane. Ni₂(L-asp)₂bipy@Pebax-20 exhibits a CO_2 permeability of 120.2 barrers with an enhanced CO_2/H_2 selectivity of 32.88 contrasted with 55.85 barrers and 1.729 of the pure membrane, which surpasses many of the reported membranes. These performances make the MMMs prepared in this work potential candidates for applications in capturing CO_2 .

ASSOCIATED CONTENT

S Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.cgd.8b00307.

Details for structural formula of Pebax polymer, optical image of pure Pebax membrane, SEM images of the MMMs, 3D structure of $Ni_2(L-asp)_2$ bipy, gas separation data of this work, and comparison with other reported work (PDF)

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The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

Notes

The authors declare no competing financial interest.

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ABBREVIATIONS

MMMs, mixed matrix membranes; MOFs, metal-organic frameworks

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